



# AtriumCalc

Version 1.0

## Atrium Smoke Control Calculator

AtriumCalc consists of a number of routines that are commonly used for analysis of atrium smoke control systems. For AtriumCalc, the term atrium is used in a generic sense to mean any large-volume space.

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[Frequently Asked Questions](#)

Enter Project Title:

### I-P Units

1: Smoke Exhaust w/ Axisymmetric Plume

2: Smoke Exhaust w/ Balcony Spill Plume

3: Smoke Exhaust w/ Window Plume

4: Preventing Plugholing

5: Airflow to Control Smoke

### SI Units

1: Smoke Exhaust w/ Axisymmetric Plume

3: Smoke Exhaust w/ Balcony Spill Plume

3: Smoke Exhaust w/ Window Plume

4: Preventing Plugholing

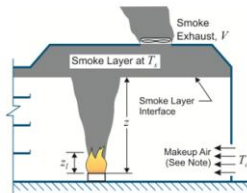
5: Airflow to Control Smoke

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Project: Atrium in Our Favorite Building, 10 Main Street, Kloteville, NY  
Routine 1: Atrium Smoke Exhaust with an Axisymmetric Plume



Notes:  
1. Makeup air is shown as being supplied by an opening or openings to the outside, but it can also be supplied by mechanical fans.  
2. For calculating the volumetric flow rate of smoke exhaust, a value of  $K_s = 1.0$  needs to be used except when another value of  $K_s$  is supported by test data or an engineering analysis.  
3. For smoke control design, a value of  $\chi = 0.7$  is almost always used, and other values should be supported by engineering data.

$$Q_c = \chi Q$$
$$z_i = 0.533 Q_c^{2/5}$$
$$m = 0.022 Q_c^{1/3} z_i^{2/3} + 0.0042 Q_c \quad \text{for } z > z_i$$
$$m = 0.0208 Q_c^{1/3} z \quad \text{for } z \leq z_i$$
$$T_s = T_a + \frac{K_s Q_c}{m C_p}$$
$$\rho_s = \frac{144 p_{atm}}{R(T_s + 460)}$$
$$V' = 60 m / \rho_s$$

where  
 $C_p$  = specific heat (0.24 Btu/lb-°F).

$$Q = \text{heat release rate of the fire (Btu/s).}$$
$$Q_c = \text{convective portion of heat release rate of fire (Btu/s).}$$
$$z = \text{distance from base of fire to smoke layer interface, (ft).}$$
$$z_i = \text{limiting elevation (ft).}$$
$$m = \text{exhaust mass flow (lb/s).}$$
$$R = \text{gas constant (53.34 ft lb/lbm}^{\circ}\text{R).}$$
$$T_s = \text{smoke layer temperature (}^{\circ}\text{F).}$$
$$T_a = \text{ambient or outdoor temperature (}^{\circ}\text{F).}$$
$$K_s = \text{fraction of convective HRR in smoke layer.}$$
$$\rho_s = \text{smoke density (kg/m}^3\text{).}$$
$$p_{atm} = \text{atmospheric pressure (psi).}$$
$$V' = \text{volumetric flow of smoke exhaust (cfm).}$$
$$\chi = \text{convective fraction (dimensionless).}$$

Input:  $Q = 3,500$  Btu/s  
 $z = 40.00$  ft  
 $T_a = 92.0$  °F  
 $p_{atm} = 14.70$  psi  
 $K_s = 1.0$  (See note 2 above)  
 $\chi = 0.70$  (Almost always 0.70)

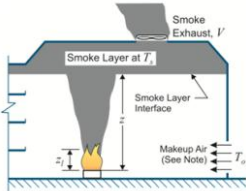
Output:  $Q_c = 2,450$  Btu/s  
 $z_i = 12.09$  ft  
 $m = 149.0$  lb/s  
 $T_s = 160.5$  °F  
 $\rho_s = 0.06396$  lb/ft<sup>3</sup>  
 $V' = 139,822$  cfm

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Project: Atrium in Our Favorite Building, 10 Main Street, Klotzeville, NY  
Routine 1: Atrium Smoke Exhaust with an Axisymmetric Plume

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Notes:

1. Makeup air is shown as being supplied by an opening or openings to the outside, but it can also be supplied by mechanical fans.
2. For calculating the volumetric flow rate of smoke exhaust, a value of  $K_z = 1.0$  needs to be used except when another value of  $K_z$  is supported by test data or an engineering analysis.
3. For smoke control design, a value of  $X = 0.7$  is almost always used, and other values should be supported by engineering data.

$Q_t = \chi Q$   
 $z_i = 0.166 Q_t^{2/5}$   
 $m = 0.071 Q_t^{1/3} z_i^{5/3} + 0.0018 Q_t$  for  $z > z_i$   
 $m = 0.032 Q_t^{1/3} z$  for  $z \leq z_i$   
 $T_s = T_a + \frac{K_z Q_t}{m C_p}$   
 $\rho_s = \frac{p_{atm}}{R(T_s + 273)}$   
 $V = m / \rho_s$   
 where  $C_p$  = specific heat (1.0 kJ/kg-°C).

$Q$  = heat release rate of the fire (kW).  
 $Q_t$  = convective portion of heat release rate of fire (kW).  
 $z$  = distance from base of fire to smoke layer interface, (m).  
 $z_i$  = limiting elevation (m).  
 $m$  = exhaust mass flow (kg/s).  
 $R$  = gas constant (287 J/kg K).  
 $T_s$  = smoke layer temperature (°C).  
 $T_a$  = ambient or outdoor temperature (°C).  
 $K_z$  = 1 for steady smoke exhaust.  
 $\rho_s$  = smoke density (kg/m³).  
 $p_{atm}$  = atmospheric pressure (Pa).  
 $V$  = volumetric flow of smoke exhaust (m³/s).  
 $\chi$  = convective fraction (dimensionless).

**Input:**  $Q = 4,000$  kW  
 $z = 12.00$  m  
 $T_a = 30.0$  °C  
 $p_{atm} = 101,300$  Pa  
 $K_z = 1.0$  (See note 2 above)  
 $\chi = 0.70$  (Almost always 0.70)

**Output:**  $Q_t = 2,800$  kW  
 $z_i = 3.97$  m  
 $m = 67.98$  kg/s  
 $T_s = 71.2$  °C  
 $\rho_s = 1.025$  kg/m³  
 $V = 66.3$  m³/s

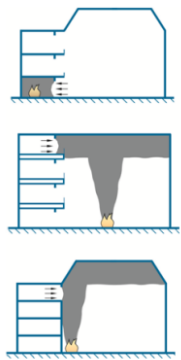
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### Airflow to Control Smoke



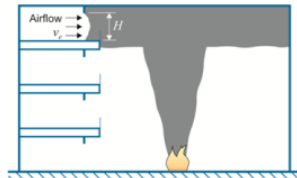
Airflow to a Communicating Space  
 Airflow to the Smoke Layer  
 Airflow to the Plume

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Project: Atrium in Our Favorite Building, 10 Main Street, Kloteville, NY  
Routine 5B: Airflow to Control Smoke Flow from the Smoke Layer



Notes:  
1. Air supply to the communicating space is not shown.  
2. The smoke exhaust from the atrium and the makeup air to the atrium are not shown.  
3. Airflow is not to be used to control smoke flow when the calculated value of  $v_a$  is greater than 200 fpm.

$$v_a = 38 \left( gH \frac{T_f - T_o}{T_f} \right)^{1/2}$$

where

$A$  = area of opening ( $\text{ft}^2$ ).  
 $g$  = acceleration of gravity ( $32.2 \text{ ft/s}^2$ ).  
 $H$  = height of opening (ft).  
 $T_f$  = temperature of smoke ( $^{\circ}\text{R}$ ).  
 $T_o$  = ambient temperature ( $^{\circ}\text{R}$ ).  
 $V$  = volumetric rate of airflow ( $V = v_a A$ ) (cfm).  
 $v_a$  = limiting average air velocity (fpm).

Note: The temperatures,  $T_f$  and  $T_o$ , can be determined from routine 1, 2 or 3.

<b>Input:</b>	$H =$	<input type="text" value="8.00"/>	ft	<b>Output:</b>	$v_a =$	<input type="text" value="157.5"/>	fpm
	$T_o =$	<input type="text" value="72.0"/>	$^{\circ}\text{F}$		$V =$	<input type="text" value="7,875"/>	cfm
	$T_f =$	<input type="text" value="110.0"/>	$^{\circ}\text{F}$				
	$A =$	<input type="text" value="50.0"/>	$\text{ft}^2$				

Note: The limiting average air velocity does not exceed the upper limit of 200 fpm.

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